

In-Situ Measurement of Fracture Toughness using the Planing-Induced Microfracture Method



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PRCI Led Innovation on NDE for Pipe Toughness

Including

PR-335-173816-R01 Validation of In-Situ Methods for Material Property Determination

PR-610-183867-R01 Fracture Toughness via In-ditch Non-destructive Testing - Validation

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Published Pipe Toughness NDE Correlations

NDE 4-8 NDE-4C Model (Hardness + micrographs + chemistry)



NDE 2-9 Regression Models (NDTT $\delta_{chip} + r_{cup} + Al$)



It has no Been Easy... (Low TRL)



Unresolved Challenge with NDTT



Recent Modeling Research on Cutting (U. of Central Florida, Texas A&M, etc.)





MMT Technology Pivot

2015: Micromachining



2022: Planing-Induced Microfracture





Planing-Induced Microfracture



- Material is stretched and then it fractures
- There is a fractured ligament on both sides that protrudes from the cutting plane



Planing-Induced Microfracture in Action



High Pipe Toughness



Lower Pipe Toughness





General Learning Moment 1

In Elasto-Plastic Contact Mechanics,

What Does Steady State Means?

No Longer Path Dependent





Proof of Concept for the Method

Step #1: Introduce microfracture



Step #2 Scan Ligaments



Step #3 Assemble



Blade Travel Distance



Step #4: Physical Model

• According to Oh [1], there is a correlation between the fracture toughness (K_{Ic}) and the toughness measured using the area under the tensile stress-strain curve up to the elongation at break (K_f):

$$\left(K_{Ic}/\sigma_{y}\right)^{2} = \alpha \left(K_{f}/\sigma_{y}\right)^{2}$$

• K_f can be estimated using the yield strength, ultimate tensile strength (σ_u), and elongation at break (ε_f):

$$K_f \approx \varepsilon_f \left[k \sigma_y + (1-k) \sigma_u \right], \quad 0 < k < 1$$

• Hypothesis: the ligament height (LH) is linearly proportional to the elongation at break considering the material within the stretch passage is subjected to predominantly tensile stress and stretched to failure:

$$\varepsilon_f = a * LH + b$$

• **Proposed correlation between** *K*_{*Ic*} **and ligament height**:

$$K_{Ic}/\sigma_y = C_1 * [k + (1 - k)\sigma_u/\sigma_y] * LH + C_2/\sigma_y + C_3$$

[1] Oh, Gyoko. "A simplified toughness estimation method based on standard tensile data." International Journal of Pressure Vessels and Piping 199 (2022): 104733.



Validation Results





General Learning Moment 2

The direct measurement:



Indirect measurement:

Impact Energy





Benchmark Comparison

X-Axis = Direct Measurement

Using same pipe samples





The Blade Toughness Meter (BTM) Prototype



Field Prototype 2024 Q2







Test in Action

B. Island Removal



C. Ligament Analysis





>>> BTM Report (~Strain to Failure)

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Field Implementation: Two Complementary Tools





ERW Seam Testing with the Current HSD







Technology Status

- BTM is approximated twice as accurate as NDTT.
- Preliminary result from a validation test of 30 vintage pipe samples shows an <u>average</u> predicted K value within ±20% of the <u>average</u> tested value.
 - Typical practice of taking lowest value of 3 measurements to be discussed.
- A prototype unit is developed and will be used in upcoming additional validation work and field trials.
- HSD and BTM are complementary tools for a complete solution.
- The HSD today (field procedures) includes the ability to receive a report for the 85% shear transition temperature & conservative upper shelf.



Concluding Remarks

- General Learning Moment 3: fracture toughness and material strength are two different properties
- In-situ minimally invasive tests to determine pipe toughness is becoming available.
- It is a considerable and collaborative effort.
- Many opportunities to engage in 2024: Industry validation programs, PHMSA BAA, field pilot projects.









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